## GOLDENDALE ENERGY STORAGE HYDROELECTRIC PROJECT

Federal Energy Regulatory Commission Project No. 14861

Klickitat County, Washington

# **DRAFT LICENSE APPLICATION Exhibit A: Description of the Project**

For:

FFP Project 101, LLC



December 2019

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## **Acronyms and Abbreviations**

AF	acre-feet
Applicant	FFP Project 101, LLC
BPA	Bonneville Power Administration
cfs	cubic feet per second
CGA	Columbia Gorge Aluminum
KPUD	Public Utility District No. 1 of Klickitat County, Washington
kV	kilovolt
MW	megawatt
MWh	megawatt-hour
U.S.	United States

#### 1.0 PROPOSED LOCATION AND FACILITIES

The following exhibit discusses the proposed Goldendale Energy Storage Project No. 14861 (Project) to be located near Goldendale, Washington, in Klickitat County, Washington, and Sherman County, Oregon. The proposed Project will be a new energy storage facility proposed by FFP Project 101, LLC (the Applicant).

#### 1.1 Site Description

A proposed FERC Project Boundary is shown in Figure 1.1-1, and encompasses all land necessary for access or control in order to construct and operate the Project and provide a possible Project "footprint" area where environmental and engineering studies are being undertaken. The Project is primarily located in Klickitat County, Washington. The Project Boundary aerially spans the Columbia River into Oregon, and contains an area in Sherman County where the transmission line will be located. Representative site photographs are provided in Appendix A.

#### 1.1.1 Land Ownership

The proposed Project Boundary encompasses approximately 649.3 acres of mostly private lands owned by NSC Smelter, LLC. All Project land disturbance will occur either on private lands or within an existing utility right-of-way owned by Bonneville Power Administration (BPA). Washington Department of Transportation lands in the Project Boundary will be crossed underground by the Project's tunnels. United States (U.S.) Army Corps of Engineers, BNSF, and private lands will be crossed by the Project's aerial transmission line within BPA's existing transmission right-of-way. Table 1.1-1 provides the ownership breakdown of area within the proposed Project Boundary.

Name	Area (Acres)	Area (Percent of Total)	
NSC Smelter, LLC	519.2	80%	
Department of Transportation	23.6	4%	
BPA right-of-way (Washington)			
BNSF Railway Co	1.9	0%	
U.S. Government (USACE)	16.2	2%	
Columbia River	6.5	1%	
BPA right-of-way (Oregon)			
Private Lands	73.2	11%	
U.S. Government (USACE)	1.0	0%	
Columbia River	7.8	1%	
Total	649.3	100%	

Table 1.1-1: Land Owners within the Proposed Project Boundary

BPA = Bonneville Power Administration; USACE = U.S. Army Corps of Engineers



Source: Esri - World Topographic Map; NAD 1983 HARN StatePlane Washington South FIPS 4602 Feet

#### **1.2** Existing Facilities

The Project will be a newly licensed facility, and there are no other existing hydroelectric facilities within the Project Boundary.

Existing facilities within the proposed Project Boundary include:

- The lower reservoir is proposed to be located at an area known as the West Side Surface Impoundment, which is an area associated with the Columbia Gorge Aluminum (CGA) smelter that was capped and closed in 2005 in compliance with applicable environmental laws. The impoundment has tested as having non-hazardous and non-dangerous material; however, this area will be characterized further prior to being excavated as part of the construction of the lower reservoir. Because the material is unsuitable fill, it will be excavated and properly disposed of pursuant to full characterization in collaboration with the Washington Department of Ecology (Ecology).
- Washington State Route 14 (Lewis and Clark Highway). Project tunnels will be constructed underneath the highway and will not interact or interfere with highway operations.
- Two wind turbines are inside the Project Boundary but are unrelated to the Project and will not be affected by the Project.
- Power distribution lines within the Project Boundary. Some of the wooden H-frame towers and distribution lines will be relocated to a route around the south side of the lower reservoir.

#### **1.3** Proposed Project Facilities

As illustrated in Figure 1.1-1, the proposed Project will consist of an off-stream, closed-loop pumped-storage project with an upper and lower reservoir with over 2,400 feet of maximum gross head that involve no river or stream impoundments, allowing for relatively small water conveyances. Other features include an underground water conveyance tunnel, underground powerhouse, 115 and 500 kilovolt (kV) transmission line(s), a substation/switchyard, and other appurtenant facilities. Table 1.3-1 shows a summary of the basic Project features.

Project Characteristics	
Approximate Installed Capacity	1,200 MW
Assumed Number of Units (Variable Speed)	3 x 400 MW units
Assumed Average Gross Static Head	2,360 feet
Assumed Usable Storage Volume	7,100 AF
Approximate Energy Storage	14,745 MWh
Approximate Hours of Storage @ 1,200 MW	12 hours
Underground Powerhouse	
Rated Head (Gross)	2,360 feet
Max Flow Generating Mode	8,280 cfs
Max Flow Pumping Mode	6,700 cfs

Table 1.3-1: Project Features Summary

AF = acre-feet; cfs = cubic feet per second; MW = megawatt; MWh = megawatt-hour

Initial fill water and periodic make-up water will be purchased from Klickitat Public Utility District (KPUD) using a KPUD-owned conveyance system and municipal water right.

The proposed Project will consist of the following new facilities:

- Upper and lower reservoirs;
- Water conveyance system;
- Underground power house and appurtenant equipment; and
- Transmission interconnection to BPA's John Day Substation.

The Project will utilize variable-speed, pump-turbine generator units and provide balancing services and renewable energy flexible capacity to utilities in the Pacific Northwest and potentially California to decarbonize the electric power system cost-effectively. Reservoirs will be entirely on private land without aquatic impacts to the Columbia River or associated riparian habitats. Water for the Project will be leased from Public Utility District No. 1 of Klickitat County (KPUD), who owns an existing water right and conveyance system adjacent to the proposed Project. The Project's lower reservoir area is located on lands that previously housed the CGA smelter (also known as Harvey Aluminum, Martin Marietta Aluminum, Commonwealth Aluminum, or Goldendale Aluminum). This facility was a primary aluminum reduction smelter that generally operated from 1969 to 2003, with a few periods when the plant shut down or had limited operation.

#### **1.4** New Dams and Reservoirs

Preliminary embankment volumes were estimated using three-dimensional CAD software. All dams were assumed to be concrete-faced rockfill structures with a crest width of 25 feet, side slopes of 1.5H:1V,<sup>1</sup> 10 feet of freeboard, and 20 feet of foundation preparation (undercut). Material take-off estimates were calculated for each dam structure assuming a crest elevation 10 feet higher than the maximum reservoir elevation. Table 1.4-1 is a summary of estimated dam, reservoir, and embankment features.

<sup>&</sup>lt;sup>1</sup> The slope ratio (H:V) formula is H:V, where HD is the horizontal distance and VD is the vertical distance.

Lower Reservoir Embankment	
Туре	Concrete-faced rockfill embankment ring dike
Height	Approximately 205 feet (max)
Length	Approximately 6,100 feet (max)
Crest Elevation	590 feet
Fill volume	6,700,000 CYs
Lower Reservoir	
Surface Area at Maximum Pool	Approximately 63 acres
Active Storage Capacity	7,100 AF and 14,745 MWh
Maximum Normal Pool Elevation	580 feet
Upper Reservoir Embankment	
Туре	Concrete-faced rockfill embankment ring dike
Height	Approximately 175 feet (max)
Length	Approximately 8,000 feet (max)
Crest Elevation	2,950 feet
Upper Reservoir	
Surface Area at Maximum Pool	Approximately 61 acres
Active Storage Capacity	7,100 AF and 14,745 MWh
Maximum Normal Pool Elevation	2,940 feet

Table 1.4-1: Dams, Reservoirs, and Embankments

AF = acre-feet; cfs = cubic feet per second; CY = cubic yard; MW = megawatt; MWh = megawatt-hour

In addition to the features included Table 1.4-1 above, other features that will be evaluated during the final design include (but are not limited to) low-level outlet size and location (if required), reservoir liner type, and freeboard. The final arrangement of Project features will be based on required studies of topography, geology, hydrology seismic hazard consideration, functional requirements, and appearance.

#### **1.5 Project Design Alternatives**

The original JD Pool Project alternative (see Exhibit B) was refined into the current overall arrangement for the Goldendale Energy Storage Project based on the recommendations described above. The rated Project capacity remained 1,200 megawatts (MW), which is considered most appropriate for the site and market conditions. Three energy storage alternatives were evaluated for this revised arrangement to allow evaluation of the cost-benefit of various reservoir sizes.

- Alternative 1: Active storage of 7,100 acre-feet (AF) allowing for approximately 12 hours of continuous run time at full generating output of approximately 1,200 MW. This alternative is presented in Figure 1.5-1.
- Alternative 2: Active storage of 11,800 AF allowing for approximately 20 hours of continuous run time at full generating output of approximately 1,200 MW. This alternative is presented in Figure 1.5-2.
- Alternative 3: Active storage of 4,800 AF allowing for approximately 8 hours of continuous run time at full generating output of approximately 1,200 MW. This alternative is presented in Figure 1.5-3.

Figure 1.5-4 shows the Project profile that is representative of all the above alternatives.

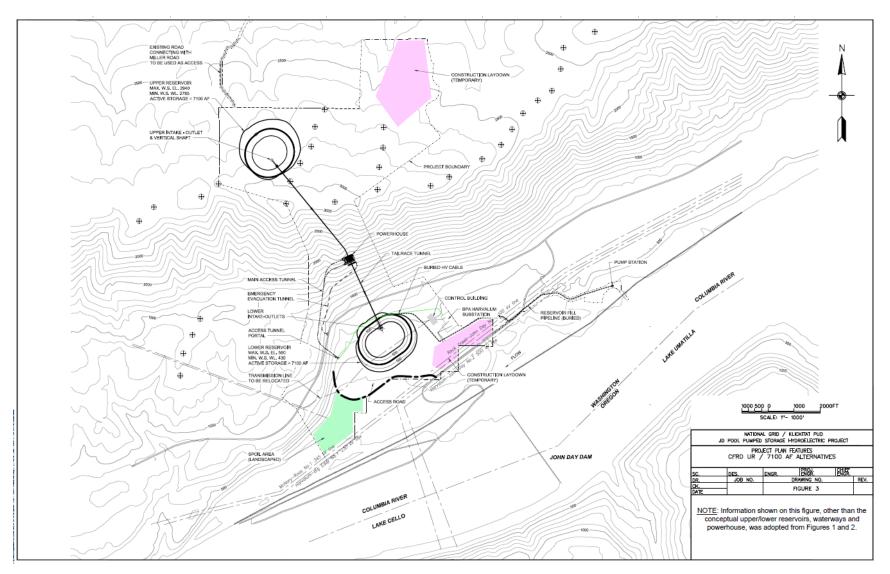


Figure 1.5-1: Goldendale Energy Storage Project General Arrangement—Alternative 1—Plan

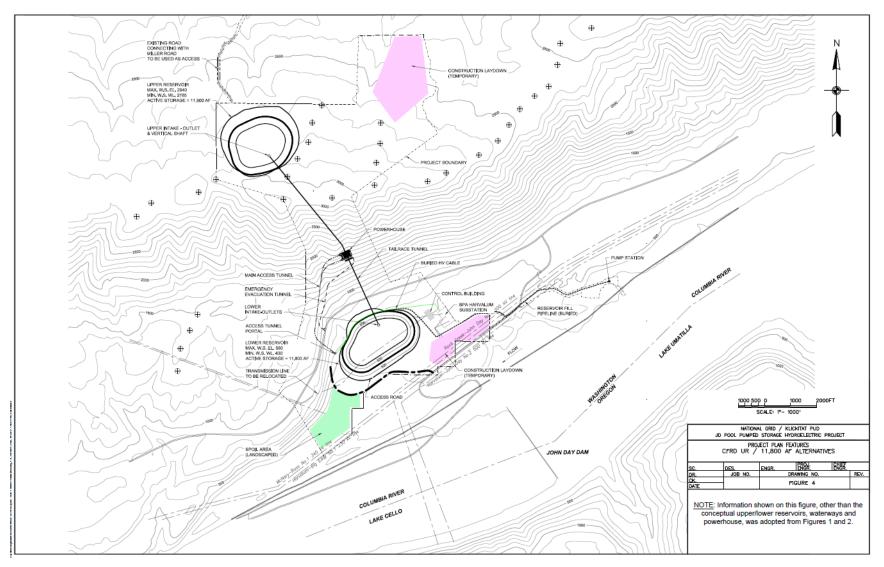


Figure 1.5-2: Goldendale Energy Storage Project General Arrangement—Alternative 2—Plan

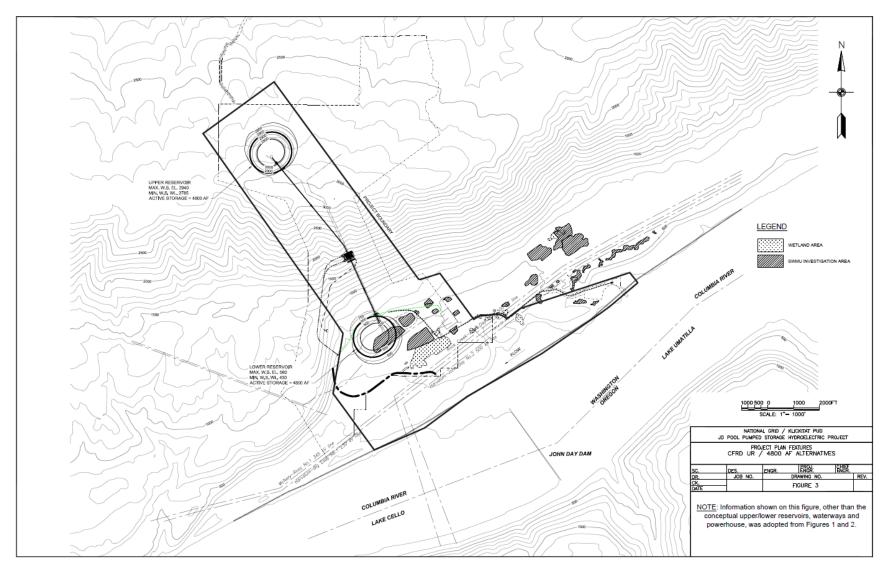


Figure 1.5-3: Goldendale Energy Storage Project General Arrangement—Alternative 3—Plan

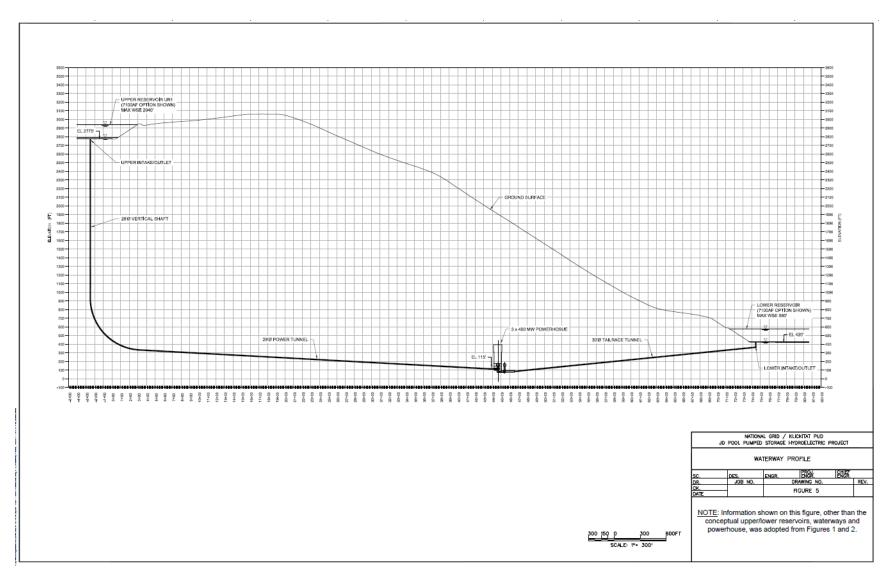


Figure 1.5-4: Goldendale Energy Storage Project General Arrangement—Typical Profile

#### **1.5.1** Selected Alternative Arrangement

Ultimately, the Project team selected Alternative 2 above (Figure 1.5-2) with an active storage size of 7,100 AF of water representing an energy storage capacity of approximately 12 hours of 1,200 MW of power, or approximately 14,745 megawatt-hours. This selected reservoir size and energy storage will balance the regional need for capacity while still providing sufficient storage capacity to facilitate load shifting and energy arbitrage.

#### 2.0 DESIGN OF WATER MANAGEMENT

A nominal (minimal) reservoir dewatering system was assumed necessary to facilitate reservoir construction. The reservoirs will be lined to prevent seepage/leakage.

There is no contributing drainage basin other than the reservoirs themselves, and both upper and lower reservoirs were assumed to contain identical active storage volumes. In the extremely unlikely event of an overpumping scenario, the water level in the lower reservoir will quickly result in a lack of water for the pumps, which, consequently, will shut off and limit any overpumping to very small volume. For these reasons, it is assumed that a spillway will not be required at either the upper or the lower reservoir. In addition, the lower reservoir will be sized to also contain, in addition to the active storage volume, the dead storage of the upper reservoir and the volume of water within the conveyance system.

#### 3.0 TURBINES GENERATORS AND POWERHOUSE

The rated (average) gross head of the Project is 2,360 feet, and the estimated maximum generating discharge is 8,280 cubic feet per second. The rated total installed capacity is 1,200 megawatt (MW) ( $3 \times 400$  MW). The Project will utilize Francis-type variable-speed, pump-turbine units with an overall cycle efficiency for pumping and generating of approximately 80 percent and a power factor of 0.9. The estimated annual generation for 8 hours a day, 7 days a week is 3,500 gigawatt-hours. Economic modeling, cost-benefit analysis, system need, and market will determine the final optimal size and configuration.

The powerhouse will be located underground between the upper and lower reservoirs in order to minimize the rock cover needed for tunnels. The location will be largely dictated by maximum unit centerline elevation (submergence below minimum normal lower reservoir level), geological characteristics, construction constraints and cost-related preferences associated with tunneling, and an acceptable hydraulic layout and configuration of the water conveyance tunnels. Intermediate step-up transformers (18/115 kV) will be housed in a separate transformer gallery cavern adjacent to the underground powerhouse. The same cavern may also house the draft tube gates. Table 3-1 shows estimated design features of the underground water conductors and penstock.

Water Conveyance Segment	Approximate Length (feet)	Assumed Finished Shape	Lining Type	Internal Diameter (feet)
Vertical shaft	2,200	Circular	Concrete	29
High pressure tunnel	3,300	Circular	Concrete	29
High pressure manifold tunnel	200	Circular	Concrete	22
Unit penstocks	600	Circular	Steel/concrete	15
Draft tube tunnel	200	Circular	Steel	20
Low pressure tunnel	200	Circular	Concrete	26
Tailrace tunnel	3,200	Circular	Concrete	30

Table 3-1: Underground Water Conductors and Penstock Details

#### 4.0 TRANSMISSION LINES

High voltage (115 kV) transmission lines will be routed from the transformer gallery in a combined access and transmission tunnel to an outdoor 115/500 kV substation and switchyard near the lower reservoir, from which a 500-kV transmission line will be routed to the interconnection location.

The location, number of circuits, voltage, and configuration of the proposed Project's interconnection with the regional electric utility network will be finalized in conjunction with BPAs transmission planning group. Based on BPAs 2017 Feasibility Study for the proposed Project, the John Day Substation is the preferred connection point for interconnection into BPA's transmission system. Additional details will be developed during the design phase of the proposed Project.

#### 5.0 OTHER FEATURES

The embankments forming the upper and lower reservoirs will include instrumentation such as movement monuments, extensioneters, and piezometers (as well as other instrumentation) to monitor the performance of the structures at all times.

#### 6.0 PROPOSED PROJECT CAPACITY AND PRODUCTION POTENTIAL

The powerhouse is planned to include three reversible, variable speed pump/turbine motor/generator units, each having a rated generating capacity of 400 MW for a total installed rated capacity of 1,200 MW. As a closed-loop pumped storage plant, the plant capacity (1,200 MW) will be dependable capacity. The upper reservoir will be capable of storing approximately 14,745 megawatt-hours of energy. The rated (average) gross head of the Project is 2,360 feet and the estimated maximum discharge is 8,280 cubic feet per second. Economic modeling, cost-benefit analysis, system need, and market will determine the optimal size and configuration for Project operations. The estimated annual generation for 8 hours a day, 7 days a week is 3,500 gigawatt-hours.